



# Basics of Phased Arrays for Atmospheric and Geospace Science

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# Superposition Principle

Maxwell's Equations are Linear:

$$\mathbf{J}_1 = \frac{1}{\mu_0} \nabla \times (\mathbf{B}_1) - \epsilon_0 \frac{\partial}{\partial t} (\mathbf{E}_1)$$

$$0 = \nabla \times (\mathbf{E}_1) + \frac{\partial}{\partial t} (\mathbf{B}_1)$$

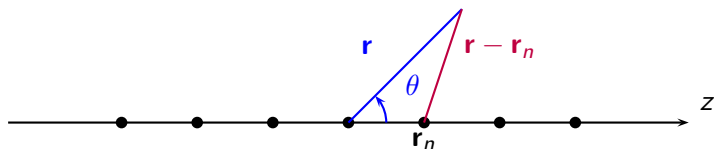
$$\mathbf{J}_2 = \frac{1}{\mu_0} \nabla \times (\mathbf{B}_2) - \epsilon_0 \frac{\partial}{\partial t} (\mathbf{E}_2)$$

$$0 = \nabla \times (\mathbf{E}_2) + \frac{\partial}{\partial t} (\mathbf{B}_2)$$

$$\mathbf{J}_1 + \mathbf{J}_2 = \frac{1}{\mu_0} \nabla \times (\mathbf{B}_1 + \mathbf{B}_2) - \epsilon_0 \frac{\partial}{\partial t} (\mathbf{E}_1 + \mathbf{E}_2)$$

$$0 = \nabla \times (\mathbf{E}_1 + \mathbf{E}_2) + \frac{\partial}{\partial t} (\mathbf{B}_1 + \mathbf{B}_2)$$

# Superposition Applied to Antenna Arrays



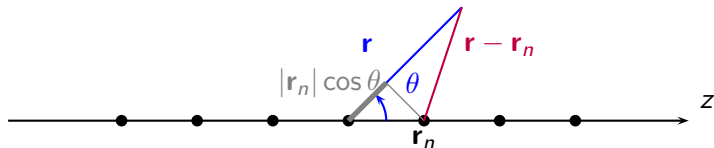
Fields radiated by single element at the origin with applied current  $I_0$ :

$$\mathbf{E} = \mathbf{E}_0 I_0 \frac{e^{-jk|\mathbf{r}|}}{|\mathbf{r}|}$$

Fields radiated by entire array:

$$\mathbf{E} = \mathbf{E}_0 \sum_{n=0}^{N-1} I_n \frac{e^{-jk|\mathbf{r} - \mathbf{r}_n|}}{|\mathbf{r} - \mathbf{r}_n|}$$

# Far Field Approximation (Fraunhofer Zone)



If  $\mathbf{r}$  and  $\mathbf{r} - \mathbf{r}_n$  are almost parallel lines:

$$\mathbf{r} - \mathbf{r}_n \approx \mathbf{r} - |\mathbf{r}_n| \cos \theta \hat{\mathbf{r}}$$

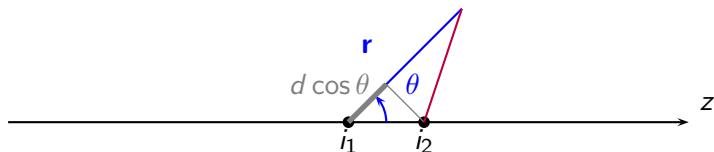
Assume  $|\mathbf{r}_n| \ll |\mathbf{r}|$ :

$$|\mathbf{r} - \mathbf{r}_n| \approx |\mathbf{r}| \text{ for demoninator terms}$$

$$-jk |\mathbf{r} - \mathbf{r}_n| \approx -jk |\mathbf{r}| + jk |\mathbf{r}_n| \cos \theta$$

$$\mathbf{E} \approx \underbrace{\mathbf{E}_0 \frac{e^{-jk|\mathbf{r}|}}{|\mathbf{r}|}}_{\text{Element Factor}} \underbrace{\sum_{n=0}^{N-1} I_n e^{jk|\mathbf{r}_n| \cos \theta}}_{\text{Array Factor}}$$

## Simple Two Element Array Example



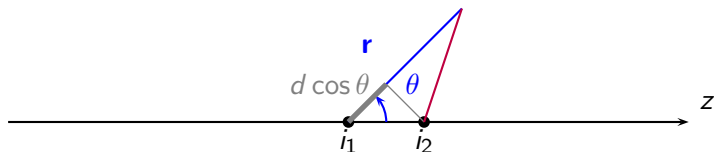
Suppose  $d = \lambda/4$  and

$$i_1(t) = \cos(\omega t)$$

$$i_2(t) = \cos\left(\omega t + \frac{\pi}{2}\right)$$

How does the radiated power vary as a function of  $\theta$ ?

# Two Element Array Example With Phasors



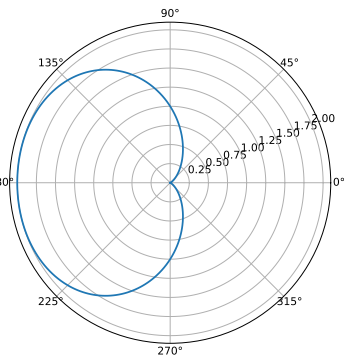
$$\tilde{l}_1 = 1 \quad \tilde{l}_2 = e^{j\pi/2}$$

$$\tilde{E} = \frac{-j\omega}{r} \tilde{l}_1 e^{-jkr} + \frac{-j\omega}{r} \tilde{l}_2 e^{-jkr + jkd \cos \theta}$$

$$= \frac{-j\omega}{r} e^{-jkr} + \frac{-j\omega}{r} e^{-jkr + jkd \cos \theta + j\pi/2}$$

$$= \frac{-j\omega}{r} e^{-jkr} \left[ 1 + e^{jkd \cos \theta + j\pi/2} \right]$$

$$\langle S \rangle \propto \frac{\omega^2}{r^2} \frac{1}{2} \left| 1 + e^{jkd \cos \theta + j\pi/2} \right|^2$$



# Active Electronically Steerable Phased Arrays

## The AMISR UHF System

### AMISR AEU = Tx/Rx Unit

- 500 W solid state transmitter
- Phasing control
- Status monitoring
- 4096 AEU's/AMISR radar face

Antenna Element Unit (AEU)



32/panel

### AMISR Panel

- 32 Antenna Element Units arranged in hexagonal pattern
- 3.5 x 2 meters; 19.8 dBi / panel
- 16 kW peak power per panel
- Basic system building block for AMISR
- Embedded linux controller



Panel (with PCU)



Face



Utility Distribution Unit (UDU)



AMISR Control System (ACS)

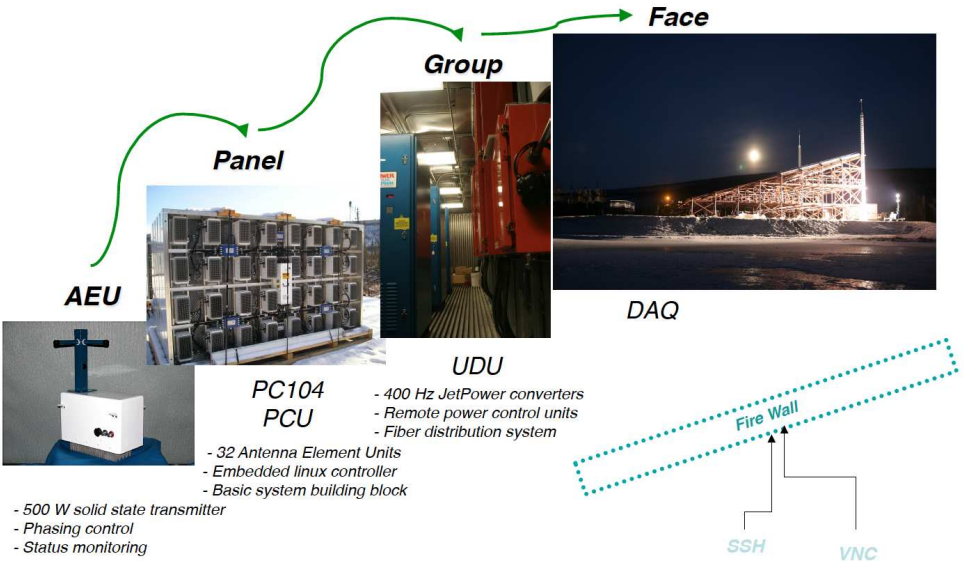
### AMISR UDU

- 400 Hz JetPower converters
- Remote power control units
- Fiber distribution system

### AMISR ACS

- Flexible transmit and receive system
- Completely remotely controlled
- Experiments run off a scheduler

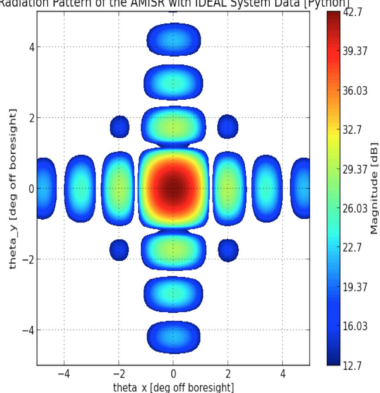
# Advanced Modular Incoherent Scatter Radar



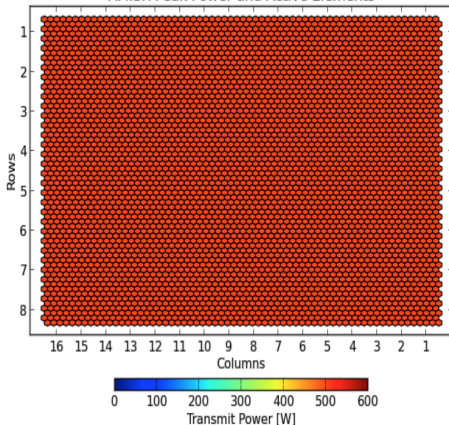


# Ideal AMISR Radiation Pattern

Radiation Pattern of the AMISR with IDEAL System Data [Python]

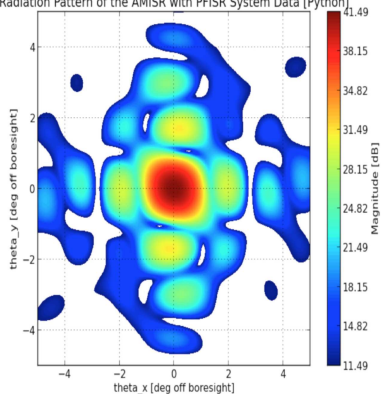


AMISR Peak Power and Active Elements

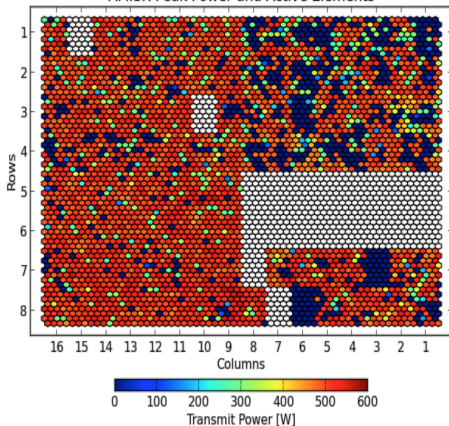


# AMISR Graceful Degradation

Radiation Pattern of the AMISR with PFISR System Data [Python]



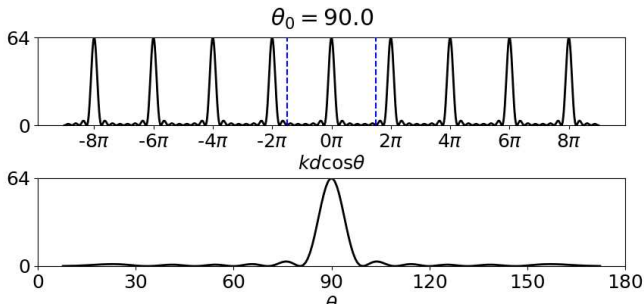
AMISR Peak Power and Active Elements



# Steering Limits and Grating Lobes

- $d < \lambda/2 \rightarrow kd < \pi$ : No grating lobes will ever appear
- $\lambda/2 < kd < \lambda \rightarrow \pi < kd < 2\pi$ : Grating lobes will only appear at some steering angles
- $d > \lambda \rightarrow kd > 2\pi$ : Grating lobes will always appear

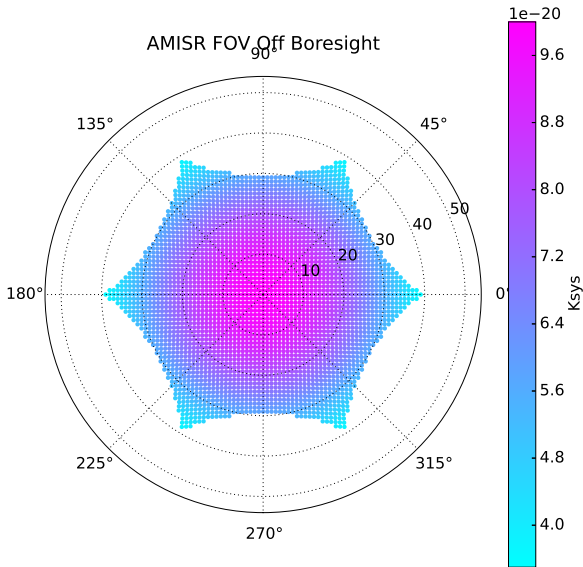
Example of linear array with  $d = 3\lambda/4$  spacing



- Maximum steering angle (for a linear array):  
$$\Delta\theta_{\max} = \left| \sin^{-1} \left( 1 - \frac{2\pi}{kd} \right) \right|$$

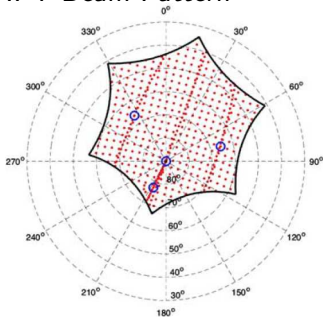
# AMISR Antenna Properties

- Hexagonal spacing with  $d \approx 3\lambda/4$
- FOV limited by grating lobe limit  $\sim 30^\circ - 40^\circ$
- Antenna gain decreases with steering angle off of boresight
- Antenna works best within  $\sim 25^\circ$  off of boresight



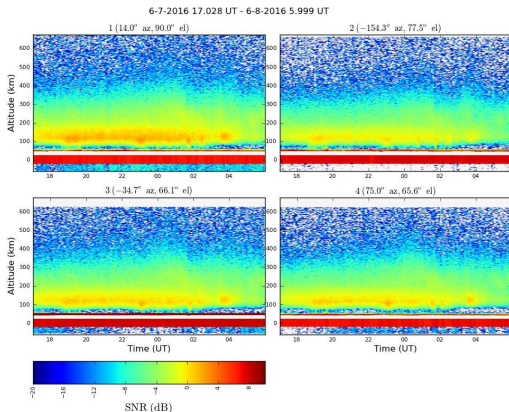
# The PFISR Up-B Compromise

## IPY Beam Pattern



The Up-B beam is close to the grating lobe limit, and therefore has reduced sensitivity.

## Reduced SNR in Up-B (Beam 2)



# Conceptual Diagram of Steering with AMISR

